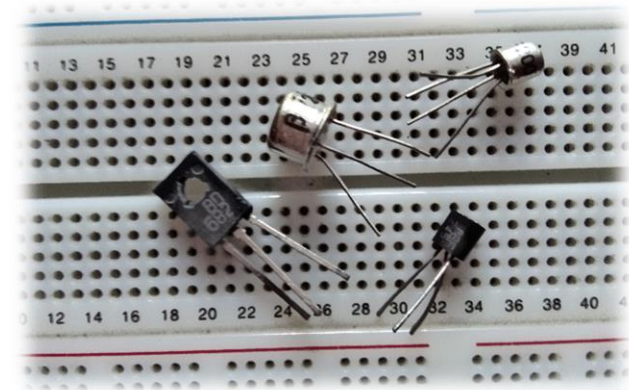




# ELECTRONIC DEVICES

Assist. prof. Laura-Nicoleta IVANCIU, Ph.D.

## C12 – BJT operation



# Contents

- Simplified structure of a BJT
- npn BJT characteristics
- Currents. Limiting the command current.
- BJT saturation
- Quiescent point of the BJT
- Operating regions
- Examples

### Previously on ED (C11):

## Transistors

= **active** semiconductor devices, with three terminals

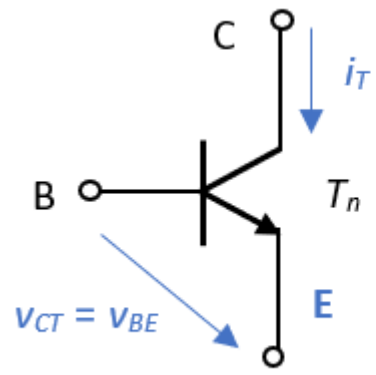
- used to amplify or switch signals
- essential components of electronic circuits
- discrete or integrated

### Operating principle:

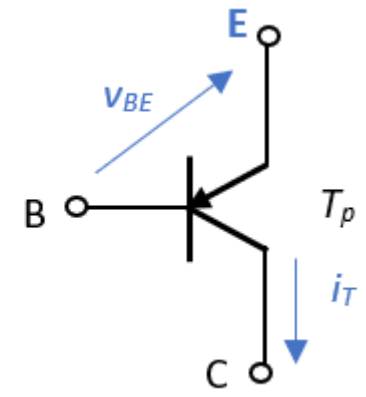
The **voltage** applied between two terminals (command) controls the **current** through the third terminal

Circuit symbols

npn



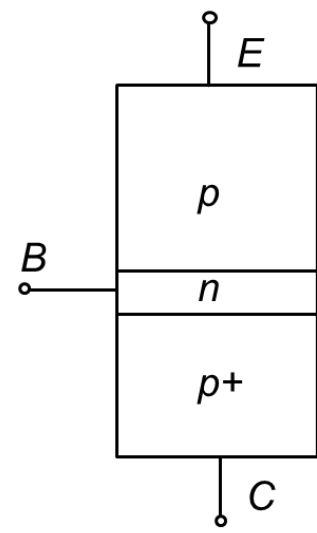
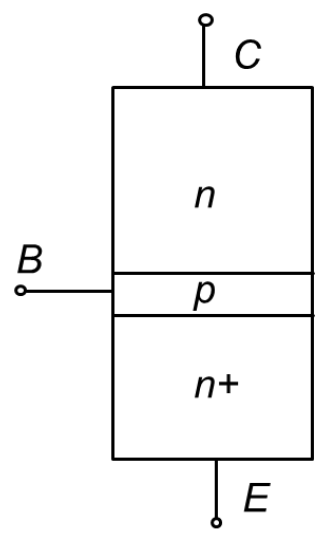
pnp



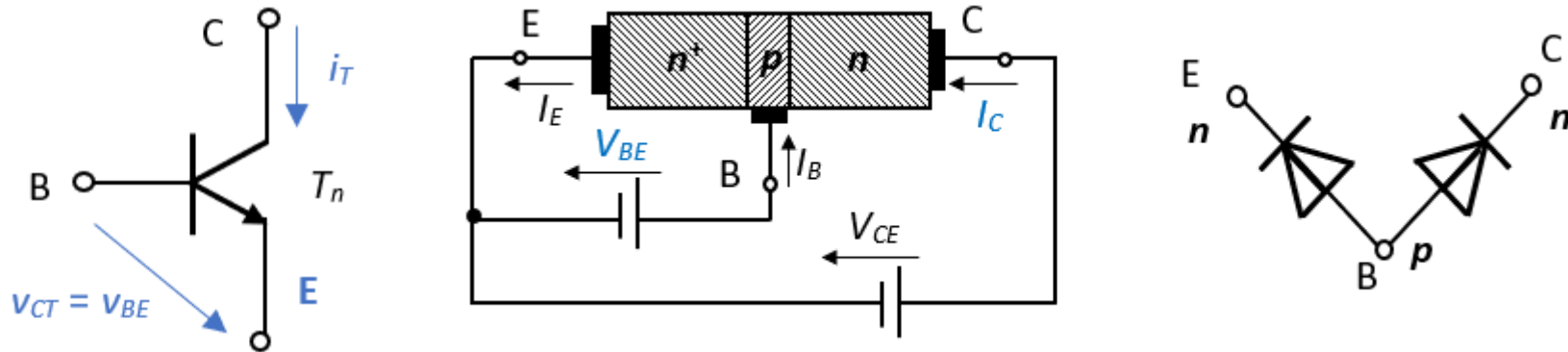
B – base, C – collector, E – emitter

The **arrow** on the **emitter** terminal indicates the direction of the **positive current**.

Simplified physical structure



## nnp

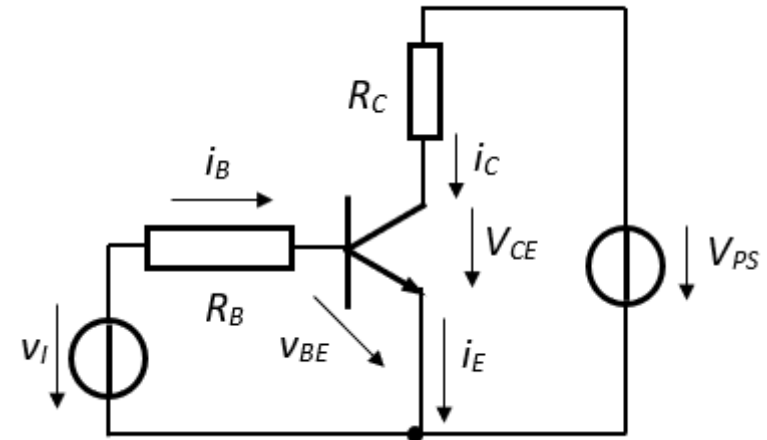


The **transistor effect** consists in a current flowing through a *reverse biased junction* (B-C) due to its interaction with a *forward biased junction* (B-E), placed in its very close vicinity.

For the transistor effect

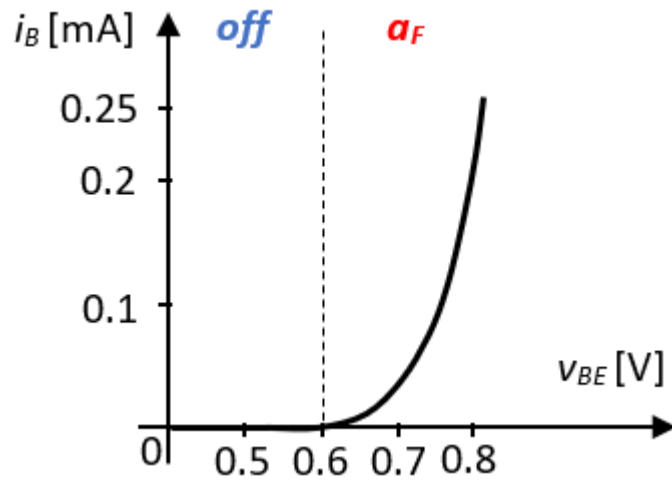
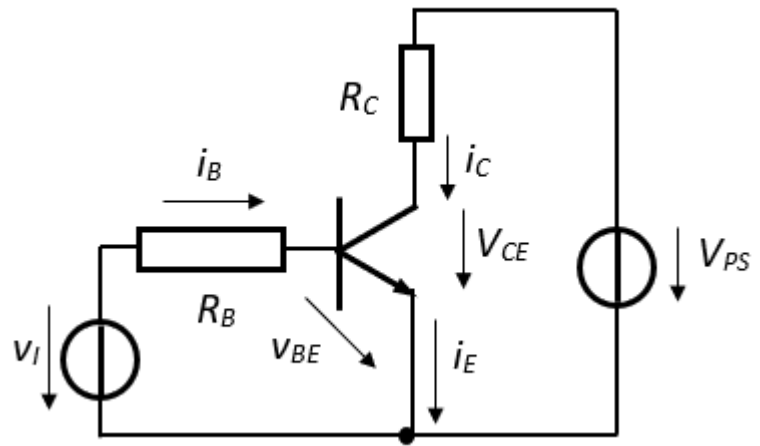
- **base** region - very thin; considerably thinner than the diffusion length of the minority carriers in the base region;
- **emitter** region - more doped than the base region
- **emitter** and **collector** regions - wider than the diffusion length of the minority carriers in these regions.

- input characteristic -  $i_B (v_{BE})$
- transfer characteristic -  $i_C (v_{BE})$



- family of output characteristics -  $i_C (v_{CE})$ , with  $v_{BE}$  and/or  $i_B$  as parameters

➤ Input characteristic



$$i_B = \frac{I_S}{\beta} e^{\frac{v_{BE}}{V_T}}$$

$I_S$  - saturation current ( $\sim$  nA - pA)

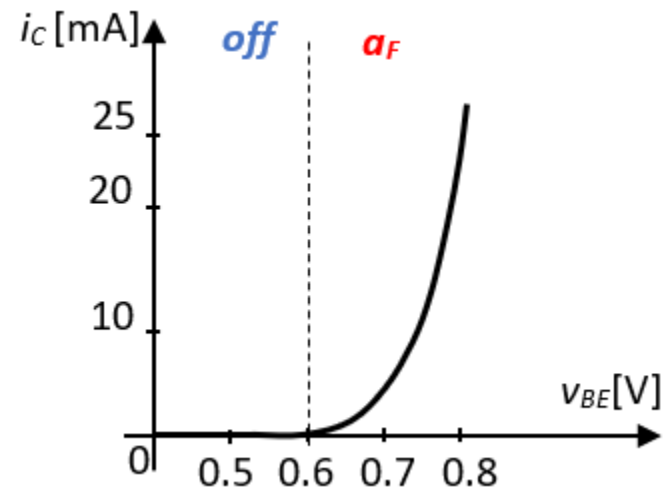
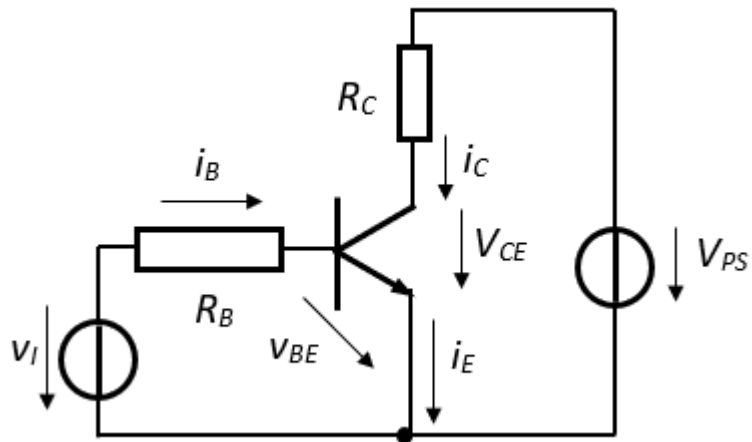
$$V_T = \frac{KT}{q} \quad \text{thermal voltage}$$

$V_T = 25\text{mV @ } 20^\circ\text{C}$

$\beta$  current gain ( $\sim$  tens, hundreds, dimensionless)

$\beta$  forward current gain factor (also denoted  $h_{FE}$  in dc or  $h_{fe}$  in ac)

➤ Transfer characteristic



$$i_B = \frac{I_S}{\beta} e^{\frac{v_{BE}}{V_T}} \quad i_C = \beta i_B \quad i_C = I_S e^{\frac{v_{BE}}{V_T}}$$

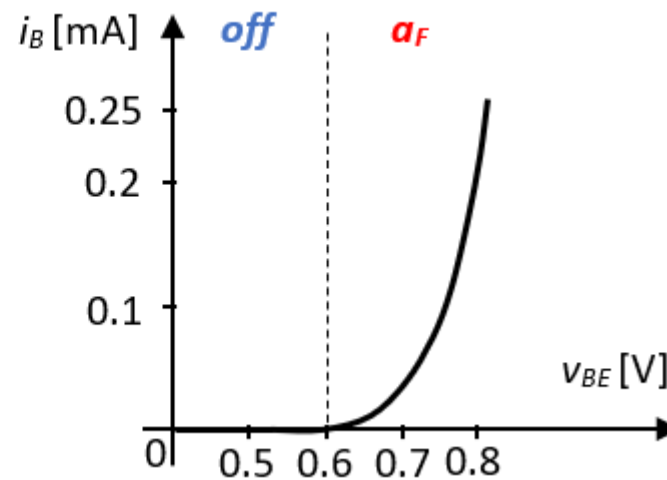
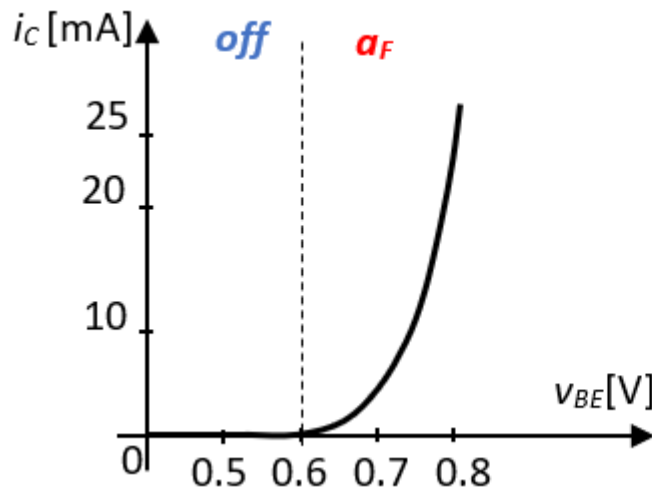


➤ Transfer and input characteristics

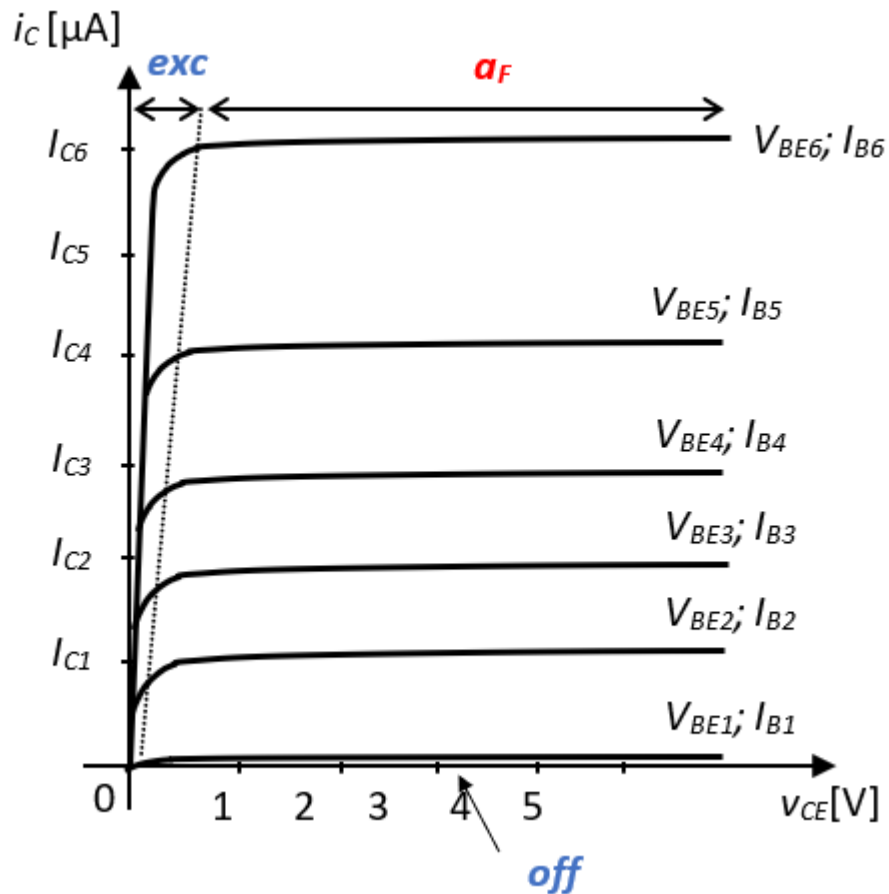
$$i_B = \frac{I_S}{\beta} e^{\frac{v_{BE}}{V_T}}$$

$$i_C = I_S e^{\frac{v_{BE}}{V_T}}$$

$$i_C = \beta i_B$$



➤ Family of output characteristics



Active forward (linear) region ( $a_F$ )

$$i_C = \beta * i_B$$

Extreme conduction (saturation) (exc)

$$i_C = i_{Cex} < \beta * i_B$$

$$V_{CEsat} \approx 0.2 \text{ V}$$

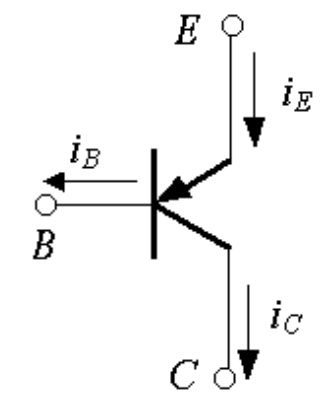
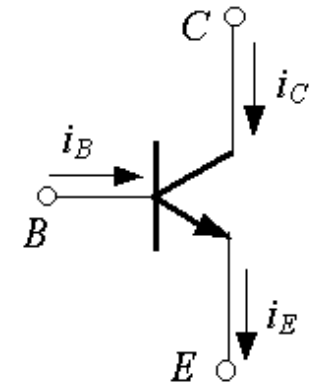
Cutoff region (off):

$$i_C = i_B = i_E = 0$$

➤ Currents

$$i_E = i_C + i_B$$

!Always valid, regardless of operating region!



In the active region ( $a_F$ ):

$$i_C = \beta i_B$$

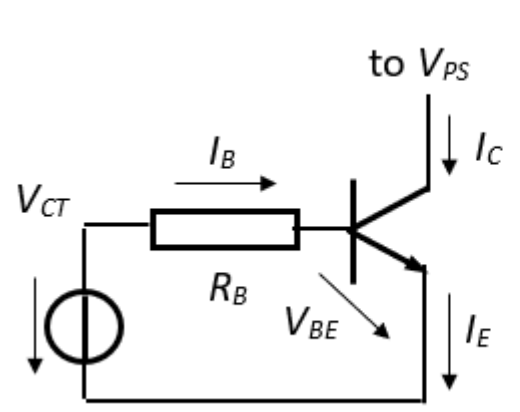
$$i_E = i_C + \frac{1}{\beta} i_C = i_C \left(1 + \frac{1}{\beta}\right)$$

$$i_E = (\beta + 1) i_B \approx \beta i_B \quad i_E \approx i_C$$

In the saturation region (exc):  $i_C < \beta i_B$

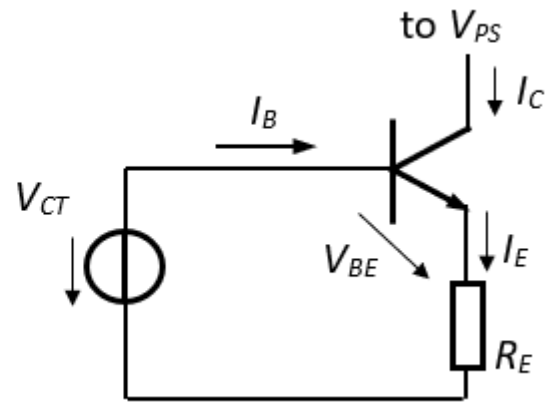
➤ Limiting the command current

Command voltage is applied between B and E, so command current is  $I_B$ .  
 Limit  $I_B$  by using a **series resistor** in B or E.



$$V_{CT} - V_{BE} - I_B \cdot R_B = 0$$

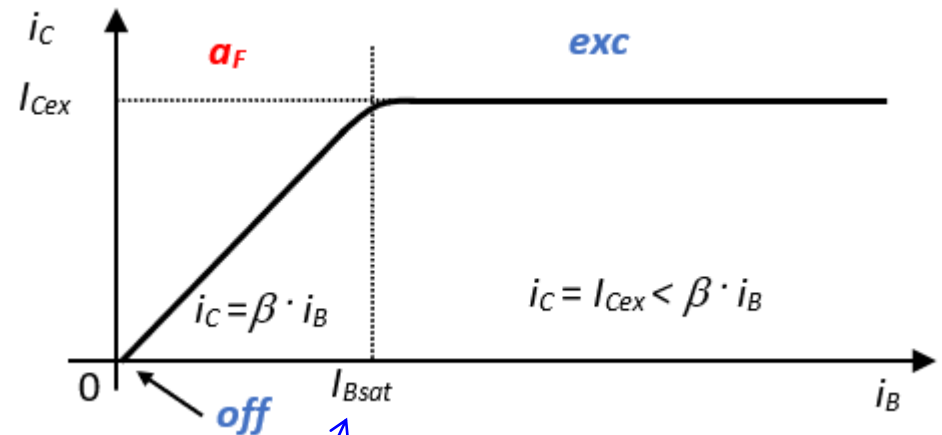
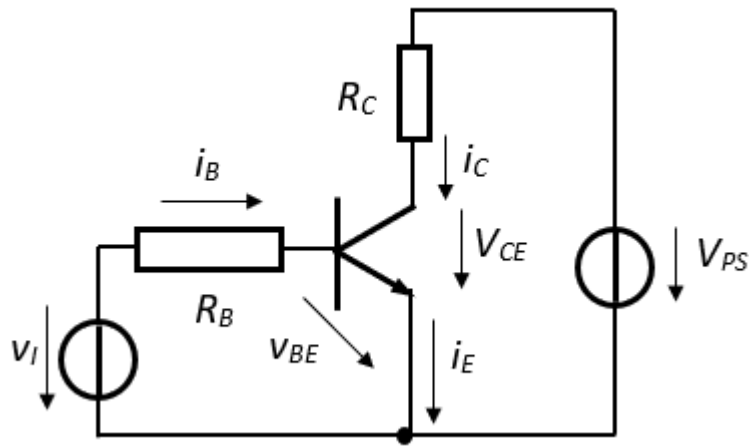
$$I_B = \frac{V_{CT} - V_{BE}}{R_B}$$



$$V_{CT} - I_E \cdot R_E - V_{BE} = 0$$

$$I_E = \frac{V_{CT} - V_{BE}}{R_E}$$

$$V_{BE} \approx 0.6 \text{ V}$$



$$i_{Cex} = \frac{V_{PS} - v_{CEsat}}{R_C} \approx \frac{V_{PS}}{R_C}$$

$$V_{CEsat} \approx 0.2 \text{ V}$$

Boundary  
(a<sub>F</sub>) - (exc)

$$i_{Bsat} = \frac{i_{Cex}}{\beta}$$

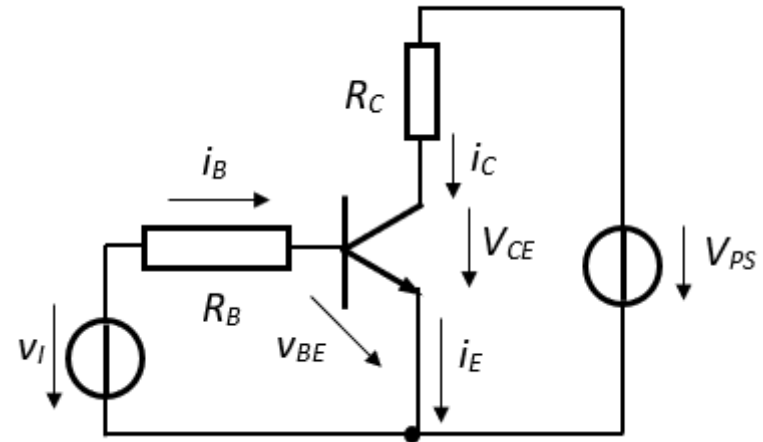
- resistors and applied voltages are chosen based on the desired region (off, a<sub>F</sub> or exc) of the BJT
- BJT can also be seen as a **current-controlled current source** ( $i_C = \beta i_B$ ), when operating in the active region (a<sub>F</sub>)

Quiescent point  $Q$  = a point on the output characteristic  $i_C(v_{CE})$  of the BJT

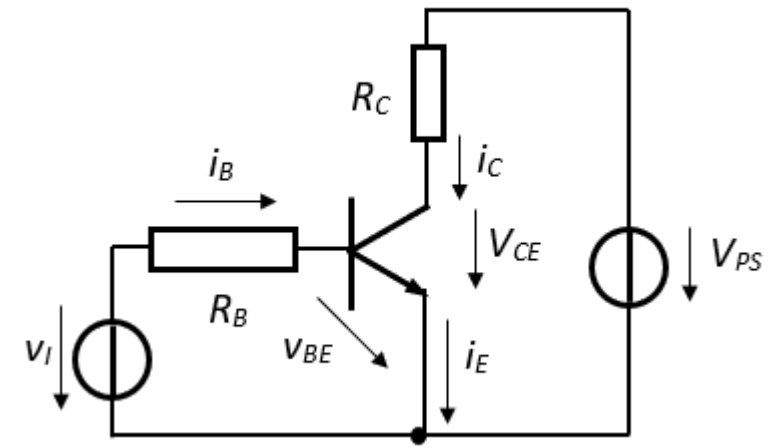
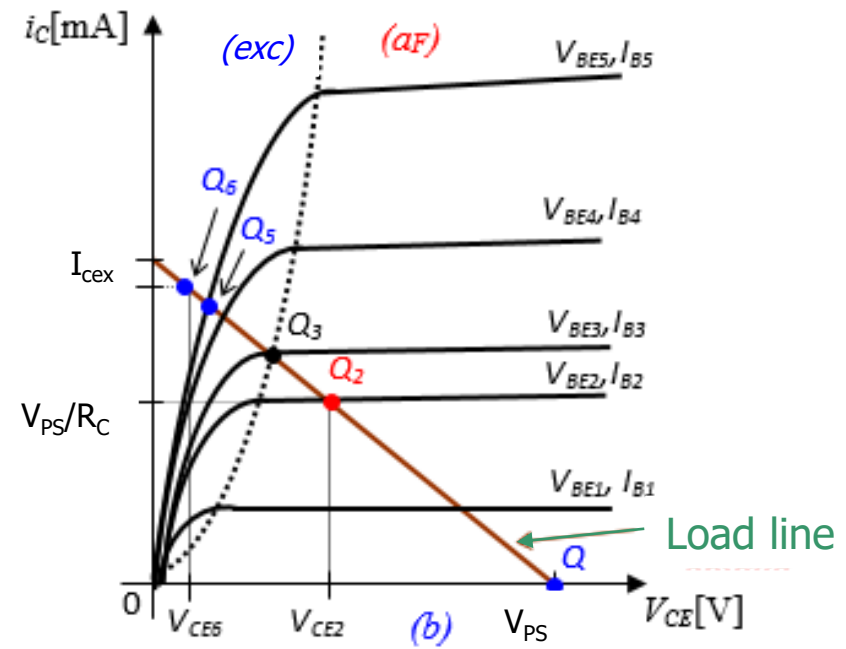
- $Q$  is defined by  $V_{CE}$  and  $I_C$
- $Q(V_{CE}, I_C)$  is at the intersection between the load line and the output characteristic corresponding to  $v_{BE}$

Load line:

$$V_{CE} = V_{PS} - R_C i_C$$



Quiescent point  $Q$  = a point on the output characteristic  $i_C(v_{CE})$  of the BJT



$Q_2(V_{CE2}, I_{C2})$

$$i_C = \beta i_B$$

$$v_{CE} = V_{PS} - R_C \cdot i_C$$

- cutoff (off)**, BJT - open switch:

$$v_{BE} < V_{BE,on} \approx 0.6 \text{ V}$$

$$I_B = I_C = I_E = 0 \text{ mA}$$

$$V_{CE} = V_{PS}$$

- extreme conduction or saturation (exc)**, BJT - closed switch:

$$v_{BE} > V_{BEsat}$$

$$I_{Bsat} = \frac{I_{Cex}}{\beta}; i_B > I_{Bsat}$$

$$I_C = I_{Cex} = \frac{V_{PS} - V_{CEsat}}{R}$$

$$v_{CE} = V_{CEsat} \approx 0.2 \text{ V}$$

- active forward or linear ( $a_f$ )**, BJT - amplifier:

$$V_{BE,on} < v_{BE} < V_{BEsat}$$

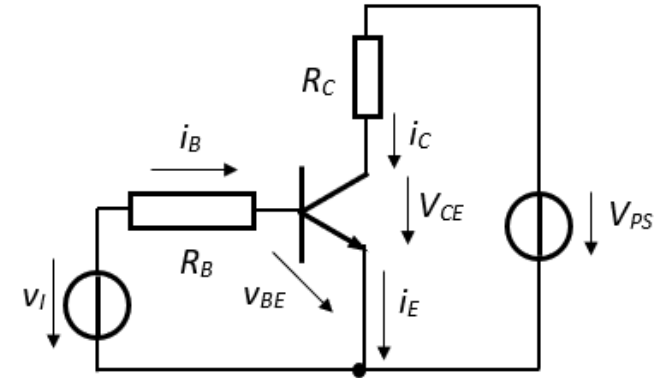
$$i_C = I_S \cdot e^{\frac{v_{BE}}{V_T}}$$

$$i_C = \beta \cdot i_B$$

$$i_E = i_B + i_C = (\beta + 1) \cdot i_B$$

$$0 \text{ mA} < i_C < I_{Cex}$$

$$0.2 \text{ V} < V_{CE} < V_{PS}$$



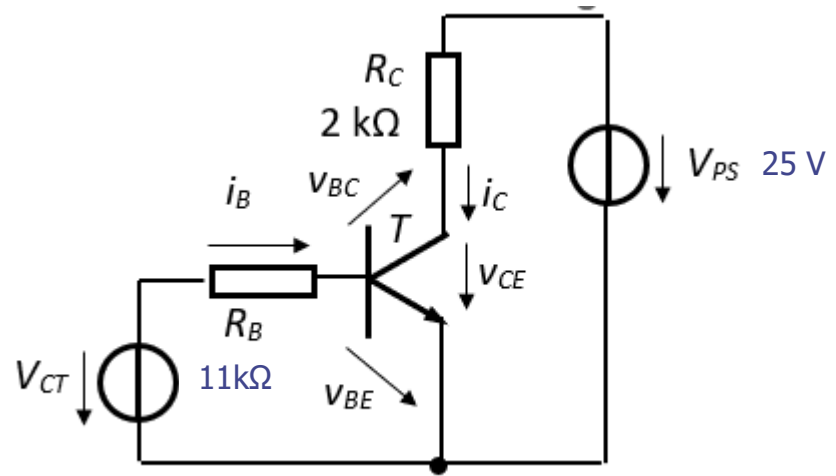


➤ Example - 1

$\beta = 100, v_{BE,on} = 0.6 \text{ V}, v_{CE,sat} = 0.2 \text{ V}$

Find the operating region and compute  $Q(v_{CE}, I_C)$  for:

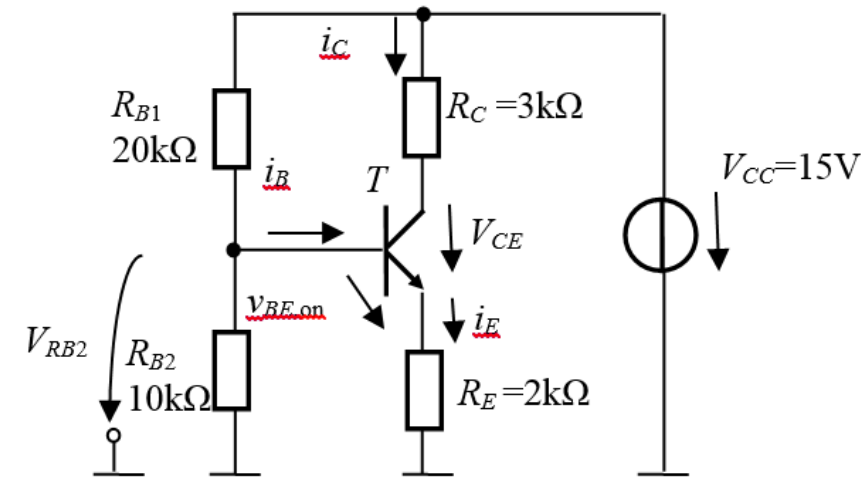
- i)  $V_{CT} = 0.4 \text{ V};$
- ii)  $V_{CT} = 1.7 \text{ V};$
- iii)  $V_{CT} = 5 \text{ V}$



➤ Example - 2

$\beta = 100, V_{BE,on} = 0.7 \text{ V}, V_{CE,sat} = 0.2 \text{ V}$

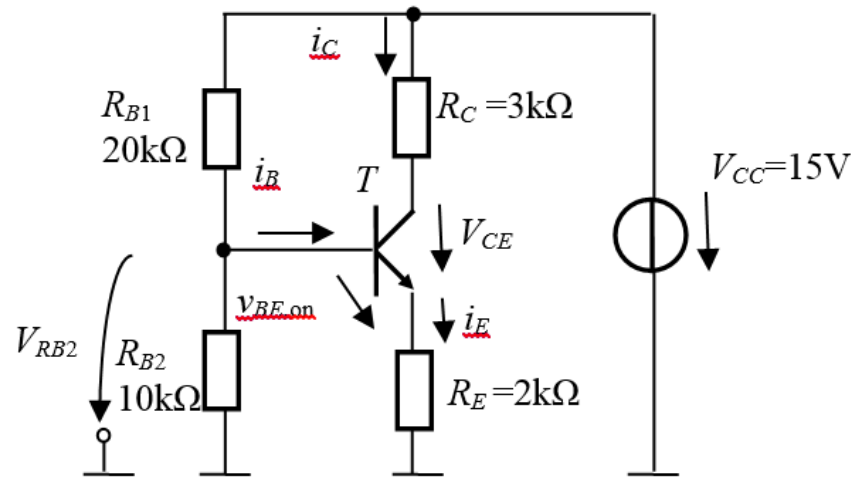
- a) Find  $Q(V_{CE}, I_C)$ .
- b) What is the operating region of T ?



➤ Example - 2

Solution:

a) Since  $I_B \ll I_C$  and  $I_E = I_C + I_B$ :  
 $I_C = I_E$



$V_{RB2}$  – obtained from the voltage divider between  $R_{B1}$  and  $R_{B2}$ , out of  $V_{CC}$

$$V_{RB2} = \frac{R_{B2}}{R_{B1} + R_{B2}} \cdot V_{CC}$$

$$V_{RB2} = \frac{10k}{30k} \cdot 15V = 5V$$

$$-V_{RB2} + v_{BE, on} + V_{RE} = 0$$

$$V_{RE} = V_{RB2} - v_{BE, on}$$

$$V_{RE} = 5 - 0.7 = 4.3V$$

$$V_{RE} = I_E \cdot R_E$$

$$I_C = \frac{V_{RE}}{R_E}$$

$$I_C = \frac{4.3V}{2k\Omega} = 2.15mA$$

➤ Example - 2

Solution:

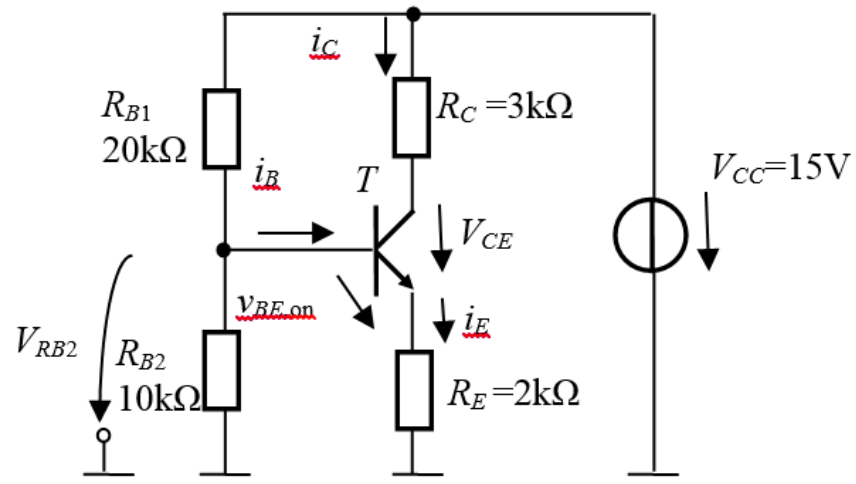
a) 
$$-V_{CC} + I_C \cdot R_C + V_{CE} + I_C \cdot R_E = 0$$

$$V_{CE} = V_{CC} - I_C \cdot (R_C + R_E)$$

$$V_{CE} = 15 - 2.15 \cdot 10^{-3} \cdot 5 \cdot 10^3$$

$$V_{CE} = 4.25V$$

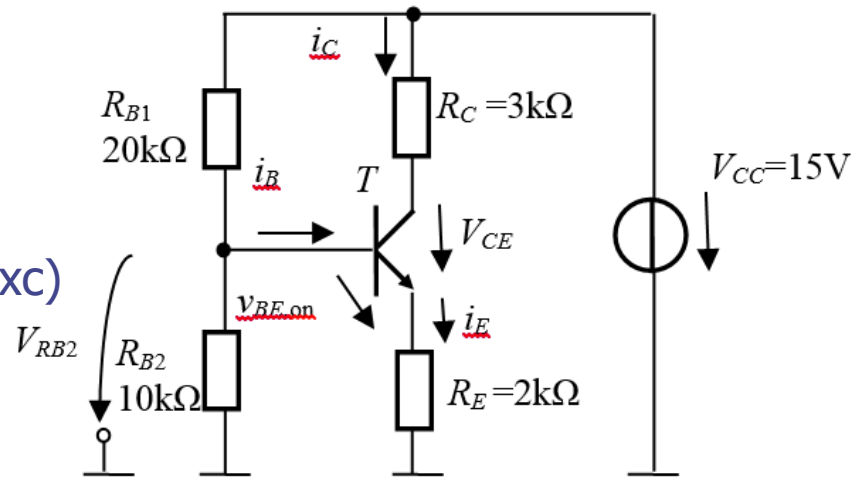
Q(4.25 V; 2.15 mA)



➤ Example - 2

Solution:

b)  $V_{C0} = V_{RB2} > V_{BE,on} \Rightarrow T$  is on, in (a<sub>F</sub>) or in (exc)



Assume T in (a<sub>F</sub>).

Compare  $i_C$  with  $i_{Cex}$  :

If  $i_C > i_{Cex}$ , the assumption was false, and T is in (exc)

If  $i_C < i_{Cex}$ , the assumption was true, and T is in (a<sub>F</sub>)

$$I_{Cex} = \frac{V_{CC} - V_{CEsat}}{R_C + R_E}$$

$$2.15 \text{ mA} < 2.96 \text{ mA}$$

$\Rightarrow$  T is in (a<sub>F</sub>)

$$I_{Cex} = \frac{15 - 0.2}{3k + 2k} = \frac{14.8}{5 \cdot 10^3} = 2.96 \text{ mA}$$

# Summary

The BJT (almost) holds no secrets from us, after investigating:

- Simplified structure of a BJT
- npn BJT characteristics
- Currents. Limiting the command current.
- BJT saturation
- Quiescent point of the BJT
- Operating regions
- Examples

**Next week:** MOSFET operation