# **MOSFET BIASING** in active region $a_F$



 $1^{st}$  version – 3 resistors, single supply



$$V_{GS} = \frac{R_{G2}}{R_{G1} + R_{G2}} V_{PS}$$

$$I_D = \beta (V_{GS} - V_{Th})^2$$

$$V_{DS} = V_{PS} - R_D I_D$$

$$(i) \text{ the current in the OP} I$$

the current in the OP, I<sub>D</sub>, depends on the transistor parameters, β and V<sub>Th</sub>
cannot assure the stability of the quiescent point.



**ODIEM 1**  

$$R_{G1}=7.6M\Omega; R_{G2}=2.4M\Omega; R_D=29.1K\Omega; V_{PS}=5V$$
  
 $V_{Th}=0.8V; \beta=500\mu A/V^2.$  OP ?  
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 $I_D$   
 $V_{GS} = \frac{R_{G2}}{R_{G1}+R_{G2}}V_{PS} = \frac{2.4}{7.6+2.4} \cdot 5 = 1.2V$   
 $I_D = \beta(V_{GS} - V_{Th})^2 = 500 \cdot (1.2 - 0.8)^2 = 80\mu A$   
 $V_{DS} = V_{PS} - R_D I_D = 5 - 29.1 \cdot 0.08 = 2.67V$   
 $V_{DSsat} = V_{GS} - V_{Th} = 1.2 - 0.8 = 0.4V$   
 $V_{DS} > V_{DSsat}$  - the transistor is in  $a_F$   
 $(V_{PS} + V_{DSsat})/2 = (5 + 0.4)/2 = 2.7V \approx V_{DS} = 2.67V$ 

The transistor is biased in the middle of its active region

 $(2.67V, 80\mu A)$ 

Resize the circuit to bias the transistor in the middle of its active region for  $I_{D1}=120\mu A$ 

 $2^{nd}$  version – 4 resistors, single supply



$$V_{GG} = \frac{R_{G2}}{R_{G1} + R_{G2}} V_{PS}$$

$$\begin{cases} V_{GS} = V_{GG} - R_S I_D \\ I_D = \beta (V_{GS} - V_{Th})^2 \end{cases}$$

- $\succ$  unknown:  $V_{GS}$  and  $I_D$
- $> 2^{nd}$  degree equations system.
- $\succ$  select the suitable  $I_D$  value

$$V_{DS} = V_{PS} - (R_D + R_S)I_D$$

2<sup>nd</sup> variant – 4 resistors, single supply - cont.



$$\begin{cases} V_{GS} = V_{GG} - R_S I_D \\ I_D = \beta (V_{GS} - V_{Th})^2 \end{cases}$$

*V<sub>GS</sub>* depends also on the drain current *I<sub>D</sub> I<sub>D</sub>* ↑, *R<sub>S</sub>I<sub>D</sub>* ↑, *V<sub>GS</sub>* ↓, *I<sub>D</sub>* ↓ the circuit
 opposes to the variation tendency of *I<sub>D</sub>*

- negative feedback due to R<sub>S</sub>
- © ensure the OP stability for variation of certain parameters

(B) increases the complexity of computational relations



 $V_{DS} = V_{PS} - I_D (R_D + R_S) =$ = 20 - 1.35(3 + 1) = <u>14.6V</u>  $V_D = ? \qquad V_S = ?$ 

- $R_{G1}=3M\Omega; R_{G2}=1M\Omega;$  $R_{D}=3K\Omega; R_{S}=1K\Omega; V_{PS}=20V$  $V_{Th}=2V; \beta=0.5mA/V^{2}.$ 
  - ? What is the OP ?

$$V_{GG} = \frac{R_{G2}}{R_{G1} + R_{G2}} V_{PS} = \frac{1}{3+1} \cdot 20 = 5V$$
$$I_D = \beta (V_{GS} - V_{Th})^2 \qquad V_{GS} = V_{GG} - I_D R_S$$

 $I_D^2 - 8I_D + 9 = 0; I_D \text{ in mA}$  $\downarrow I_{DI} = 6.65 \text{mA and}$  $I_{D2} = 1.35 \text{mA}$ 

 $I_{DI}$  is not suitable; results  $V_{GS} < 0$ 

 $I_D = I_{D2} = \underline{1.35 \text{mA}}$ 



#### Problem 3 – cont.



*MOSFET:*  $V_{Th} = 2 \text{ V}; \beta = 0.25 \text{ mA/V}^2$ ? Choose the resistances to obtain  $I_D = 1 \text{ mA}$  in the OP

 $R_D$ ,  $R_S$  also sets the gain. For now we can consider  $V_S = 7V$  across  $R_S$ :

$$R_{S} = \frac{V_{S}}{I_{D}} = \frac{7}{1} = 7 \,\mathrm{k}\Omega$$
$$R_{D} = 13 - 7 = 6 \,\mathrm{k}\Omega$$

 $V_{GG} = V_{GS} + V_S = 4 + 7 = 11 \text{V}$  $R_{G1} = 180 \text{ k}\Omega; \quad R_{G2} = 220 \text{ k}\Omega$ 

3<sup>rd</sup> version – current source, single /differential supply

- Usual in integrated circuits: biasing with *current sources*
- *I<sub>D</sub>* independent of the transistor parameters

single supply



$$I_D = I$$

$$V_{PS} = R_D I + V_{DS} - V_{GS} + V_{GG}$$

$$V_{DS} = V_{PS} - R_D I + V_{GS} - V_{GG}$$

Voltage across the current source:  $V_{GG}$  -  $V_{GS}$ 

- 3<sup>rd</sup> version current source, single /differential supply
- Usual in integrated circuits: biasing with *current sources*
- I<sub>D</sub> independent of the transistor parameters

#### differential supply



$$\pm V_{PS} = \pm 12 \mathrm{V}$$

$$R_G = 500 \text{ k}\Omega, R_D = 4.7 \text{ k}\Omega, I = 1.6 \text{ mA}$$

$$I_D = I \quad k = 0.1 \text{ mA} / \text{V}^2, \frac{W}{L} = 2, V_{Th} = 0.5 \text{ V}$$



 $V_{PS}$ 

 $R_D$ 

What is the OP?

What are the dc potentials in the terminals of the transistor?

What is the voltage drop across the dc biasing current source?